Lecture 5: Axisymmetric Madley Cells

Last learne

- Showed that RCE solution is not the correct solution in the limit of weak viscosity
 - In particular RCE Solution implies strong meridional temperature gradients which by thermal wind imply zonal wind distribution that urbates thedes theorem
 - Lerge Scale circulation must therefore develop that reduces werdional remperature gradients.
- This letter we seek to curdenstand what this "hearly invisied" axisymmetric corculation looks like

What closes this nearly invisid circulation look like?

Retaining our axisymmetric assumption. The equation for angular momentum for cready inviscid flow is,

=> velocity vectors must be perpendicular to DM

. .

M is conserved along streamlines!

Hence we have $M_{t}(\phi) = \Omega Re^{2}$ $R_{e} \cos \phi \left(u_{t} + 5 R_{e} \cos \phi \right) = 5 2 Re^{2}$

$$\begin{aligned}
\mathcal{H}_{t} &= \underbrace{SRe}_{cosp} - \underbrace{SRecosp}_{cosp} \\
&= \underbrace{SRe}_{cosp} \left(1 - \cos^{2} \mathcal{K} \right) \\
&= \underbrace{SResin^{2} \mathcal{K}}_{cosp} \\
\mathcal{H}_{t} &= \underbrace{SResinp tanp}_{p_{0}^{o}} \underbrace{\mathcal{K}}_{p_{0}^{o}} \underbrace{$$

Nour, a ssame me have hydrostatic & gradient wind halance. Allows us no derive thermal wind equation as in prev. between

$$\begin{bmatrix} 2 \sum suing u + u^{2} \tan \varphi \\ Re \end{bmatrix}_{O_{S}}^{P_{L}} = - \frac{P_{a}}{P_{e}} \frac{lmp_{r}}{\delta \varphi}, \quad \hat{T} = - \frac{l}{h_{r}} \int_{P_{r}}^{h_{r}} \int_{P_{r}}$$

Again assuming winds near the surface are weak:

Substituting the angular momentum conserving vinel.

$$2 \pi^{2} R_{e}^{2} \sin^{2} \beta \tan \beta + \pi^{2} R_{e}^{2} \sin^{2} \beta \tan^{3} \beta = -R_{u} \partial^{2} T \ln \beta \sin^{2} \beta \tan \beta = -R_{u} \partial^{2} T \ln \beta \sin^{2} \beta \tan \beta = -R_{u} \partial^{2} T \ln \beta \sin^{2} \beta \sin^{2}$$

$$\int -T_{0} = -\frac{52^{2} e^{2}}{R_{d} ln ls} \int_{0}^{l} tan^{3} d' (1 + cos^{2} d') d\beta' \qquad [hoogle this]$$

Now,

$$\int_{0}^{\psi} \tan^{3}x \left(1 + \cos^{2}x\right) dx = \int_{0}^{\psi} \tan(x) \left(1 - \cos^{2}x\right) \left(1 + \cos^{2}x\right) dx$$

$$= \int_{0}^{\psi} \tan(x) \left\{1 - \cos^{2}x\right\} dx$$

$$= \int_{0}^{\psi} \tan(x) dx + \int_{0}^{\psi} \sin(x) \cos(x) dx$$

$$= \left[1 + \tan^{2}(x)\right]_{0}^{\psi} - \left(\frac{\sin^{2}y}{2}\right)_{0}^{\psi}$$

$$= \frac{1}{2} \left\{ \frac{\sin^{2}\psi}{\cos^{2}\psi} - \frac{\sin^{2}\psi}{\cos^{2}\psi} \right\}$$

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$$Hence, \quad T(y) = T_o - \frac{s^2 Re^2}{2 Ra lnps} \left(\frac{s_1 i s^4 \phi}{c s^2 \psi} \right)$$

Mave found men remperature distribution using only anglelar momentum conservation!

Thermodynamics of Hadley cell

- · Expect Hadley cell to transport energy poleward
- . If no eddies, Hadley cell heat flux divergence must balance hear fluxes due to radiation/convection.
- · Consider simple parametersation,

$$\langle Q \rangle = - \frac{1}{T} - \frac{1}{T} \frac{1}{T}$$

Implies:
$$\int_{gbbc} \hat{T} ds = \int_{gbbc} \hat{T}^{rcc} ds$$





Calculating the Hadley cel estent

We have 2 constraints:

- 1. Continuity of mean temp. accross the Hadley cell edge:
 - Define φ_{H} as latitude of Madley cell edge: $\frac{1}{T}(\varphi_{H}) = \frac{1}{T} \frac{\partial \varphi_{H}}{\partial \varphi_{H}}$
 - 2. Energy conservation :

$$\int_{0}^{\#H} \left(\hat{T} - \hat{T}^{\text{RCE}} \right) \cos \phi \, d\phi = 0$$

Can solve for \$4 and So

For simplicity, use small angle approx.
=)
$$\sin \phi \simeq \phi$$
, $\cos \phi \simeq 1$
 $\hat{T} = \hat{T}_0 - \frac{52^2 Re^2}{2R_4} \phi^4 = \hat{T}_0 - \frac{5}{5T} \phi^4$ $(\hat{T} = 5Re^2)$
 $\hat{T} = \hat{T}_0 - \frac{52^2 Re^2}{2R_4} \phi^4 = \hat{T}_0 - \frac{5}{5T} \phi^4$ $(\hat{T} = 5Re^2)$

Constraint (2) gives:

$$\int_{0}^{\psi_{H}} \hat{\tau} - \hat{\tau}_{0}^{RCE} - \hat{s}\hat{\tau}\phi^{4} + \hat{s}\hat{\tau}^{RCE}\phi^{2} d\psi = 0$$

$$=) \quad (\hat{\tau}_{0} - \hat{\tau}_{0}^{RCE})\phi_{H} - \hat{s}\hat{\tau}\phi_{H}^{T} + \hat{s}\hat{\tau}^{RCE}\phi^{3} = 0$$

$$= \hat{s}\hat{\tau}\phi_{H}^{4} - \hat{s}\hat{\tau}^{RCE}\phi_{H}^{2} - (\hat{\tau}_{0} - \hat{\tau}^{RCE}) = 0 \quad (1)$$

Constraint (1) gives

$$\hat{\tau}_{0} - S \hat{T} \phi_{H}^{4} - \hat{T}_{0}^{2CE} + S \hat{T}^{2} \phi_{H}^{2} = 0 \qquad (2)$$

add (1) and (2)

$$\begin{pmatrix} S\tilde{T} - S\tilde{T} \end{pmatrix} \varphi_{H}^{4} + \left(S\tilde{T}^{RCE} - S\tilde{T}^{RCE} \right) \varphi_{H}^{2} = 0$$

$$\begin{pmatrix} S\tilde{T} & \varphi_{H}^{2} \\ S & \varphi_{H}^{2} \end{pmatrix} = 2 S\tilde{T}^{RCE}$$

$$\begin{pmatrix} S\tilde{T} & \varphi_{H}^{2} \\ S & \varphi_{H}^{2} \end{pmatrix} = \left(\frac{5}{5} S\tilde{T}^{RCE} \right)^{\frac{1}{2}}$$

$$[\phi_{H}] = \left(\begin{array}{c} 5 \text{ GARGE} \\ 3 \end{array} \\ \overline{3} \end{array} \\ \overline{3}^{2} R_{e}^{2} \end{array}\right)^{\frac{1}{2}}$$

Let's plug in some reasonable numbers: $P_s/\rho_t \approx 10 = h_1(P_s) = 2.3$ $sf^{RLE} \approx (100 \text{ K})$

$$|\phi_{H}\rangle = \frac{5}{3} \times \frac{100 + (2.3) \times 287}{(7.29 \times 10^{-5})^{2} (6.3 \times 10^{6})^{2}}$$

= 0.5 = 30° Surprisingly close to observed! Strength of the Hadley cell

In the Held-How theory the strength of the Hadley cell is related to its energy transport.

- In particular, we assumed that
 - 1) The Hadley all is energetically closed
 - 2) The net column heating is propurhound the decription of the temperature from its RCE value.

Together, nese assumptions imply

$$\frac{1}{R_{ecosp}} \frac{\partial F_{H}Cosp}{\partial k} = \langle Q \rangle = \frac{1}{1-\frac{1}{2}} \frac{1}{R_{ecosp}}$$

where Fy is the energy flux by the Madley cell.

Meld & Mar assumed poleward flow near the tropopouse and equatorward retrin How



Assuming the flow is concentrated in a layers near the tropopource and surface of pressure depth Sp:

$$F_{H} = \left(\int_{P_{t}-\delta_{P}}^{P_{t}} \sigma_{t} \frac{d\rho}{g} \right) h_{t} - \left(\int_{P_{s}-\delta_{P}}^{P_{s}} \sigma_{t} \frac{d\rho}{g} \right) h_{t}$$

where h is the "energy" (see below).

By mass conservation, have that

$$\int_{Pe-dp}^{Pu} \sigma_e \, dp = -\int_{Pe-\delta p}^{P} \sigma_b \, \frac{dp}{g} = 4max$$

$$=) \quad F_H = 4max \text{ Ah}$$

$$= 5max \text{ Ah}$$

$$=$$

Gross energy statication

In queesi-equilibrium <u>2h*</u> = 0 in troposphere (h is related to s, entropy) h^{*}_m = CpT + 92 + L/2[×] h^{*}_m - h_m = L_V(q^{*}-q)
Boundary layer: Ret high, q^{*}-q is small troposphere : RM hower, q^{*}-q is large

tropopause : T is low, at is small at - 2 is small



hy has minimum in mid tropogohore!

The size (and sign!) of the gross energy strahification depends on the profile of 5!

This is usually discussed in terms of the gross made stability introduced by Neelin 4 Meld (1987)

Additional complication: -> Most poleward energy transport of low lathholes is effected through ocean circulation -> But ocean circ. driven by surf. wind ctress.

Hadley all energetics is complicated. Will return to thus topic later in the course.

Held of Mon Zonal wind distribution

Tropopouse winds



Problems with Meld Hou



What is going on?

Let's rejisit the assumptions of the model: (1) Rising notion (2) poleward flow at tropopause - computer momentum conserved at equator: - shew is low (3) Return flow in BL - weak winds - M=Mp

2 possibilities



2) Need to remove angular-momentum in the descending branch How? EDDIES!